

1 **APPLICATION OF DIGITAL PHOTOGRAMMETRY TO ROCK CUT SLOPE DESIGN**  
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23 **ABSTRACT**

24  
25 To reduce future maintenance along a rockfall-prone stretch of U.S. Highway 15 on Bald  
26 Eagle Mountain near South Williamsport, the Pennsylvania Department of Transportation  
27 proposed to remove an existing rockfall fence and modify the existing cut to provide a rock  
28 catchment ditch in order to mitigate the rockfall hazard.

29 Digital photographs were used to develop a three-dimensional, digital model  
30 encompassing a 420-foot-long section of the existing rock cut. The orientations of 238 rock  
31 discontinuities visible in the model were measured. A Brunton Geotransit was used to collect  
32 additional measurements from behind the rockfall fence and to validate the model measurements.

33 Discontinuity measurements were used to analyze the potential for plane, toppling, and  
34 wedge failures, to assess the variability of dip angle and dip direction along the alignment, and to  
35 optimize the azimuth of horizontal drain holes. The digital model was used to locate the possible  
36 outcrop of clay seams encountered in rock core borings.

37 Using digital photogrammetry permitted measurement of discontinuities in higher parts  
38 of the outcrop without rappelling or free-climbing. A great volume of data was collected in a  
39 short period of time, reducing exposure to rockfalls and traffic. Discontinuities were measured  
40 over a greater area of their extent, and discontinuities having limited surface exposure were  
41 measured by digitizing their trace across the outcrop. Using digital photogrammetry reduced the  
42 potential for human error in the collection, recording, and processing of data, and facilitated  
43 performance of some of the analyses required for designing a safer rock cut slope.

44 **INTRODUCTION**

45 Rockfalls have been a recurring problem on a curved portion of U.S. Highway 15 on Bald Eagle  
46 Mountain south of Williamsport, Pennsylvania. Conditions contributing to rockfalls include  
47 bedding planes dipping obliquely toward the roadway, joints dipping steeply into the cut  
48 providing an upper release surface, steeply dipping orthogonal joints providing lateral release  
49 surfaces, and undercutting of quartzite beds as a result of differential weathering of weaker shale  
50 and siltstone beds (Figure 1).

51 Rockfalls typically occur during the late winter and early spring, when during peak  
52 freeze/thaw conditions, rockfalls may occur nearly daily or several times a week over the period  
53 of a month. Fallen rock blocks are estimated to be up to about 0.5 yard<sup>3</sup> (0.4 meter<sup>3</sup>) in size and  
54 often require a loader to move, which necessitates a lane closure. To reduce future maintenance  
55 and improve safety, the Pennsylvania Department of Transportation (PennDOT) proposed to  
56 remove an existing rockfall fence, modify the existing rock cut, and provide a rockfall catchment  
57 zone. Modification of the rock cut will also improve sight distance.

58 Rock discontinuity data were needed to perform the rock slope stability analyses required  
59 for developing revised cut slope recommendations. A Brunton or clar compass is typically used  
60 to measure rock discontinuities; however, collecting measurements can be perilous work in areas  
61 of challenging access, areas of instability, and areas of high traffic volume. Digital

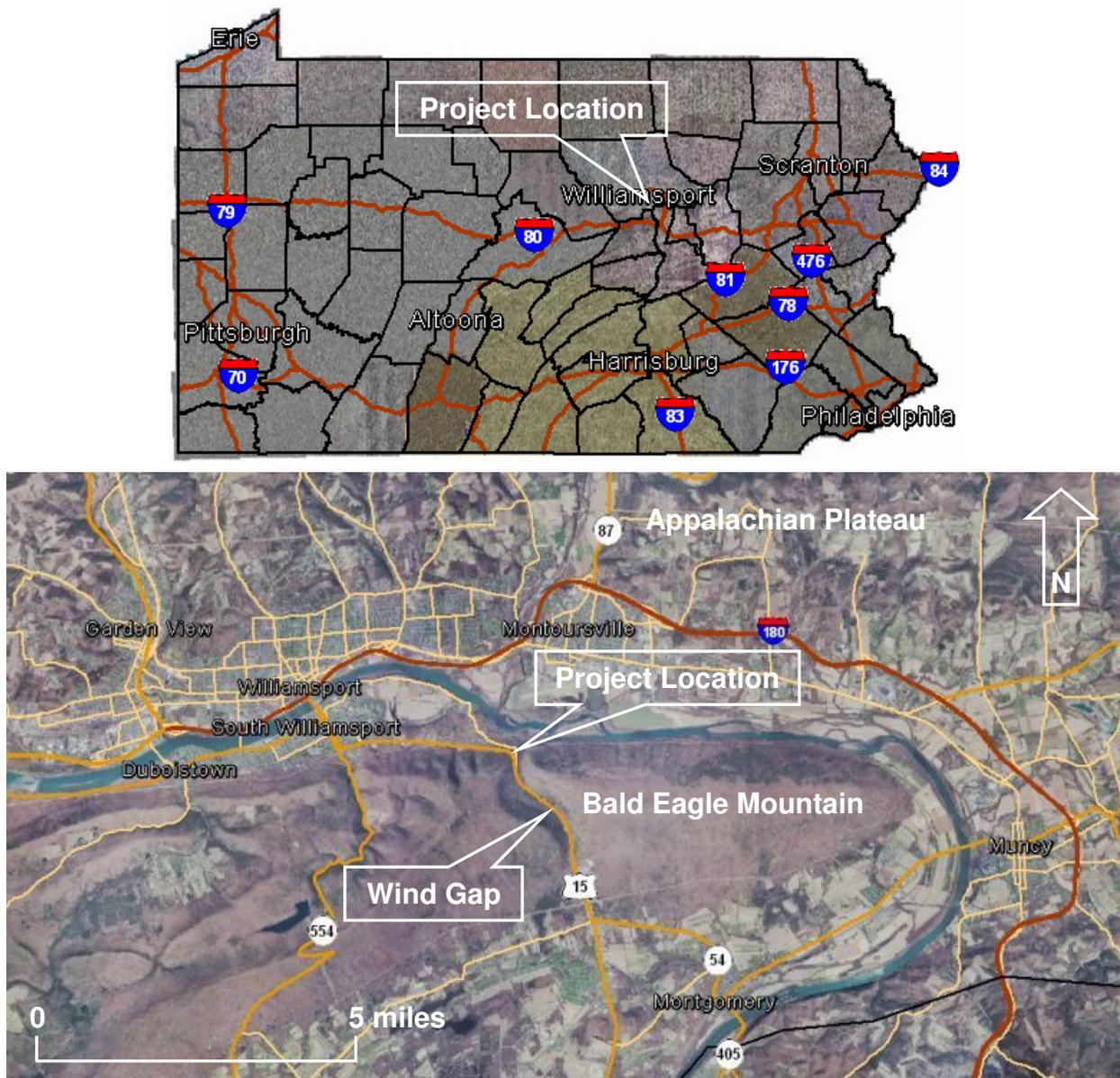


**FIGURE 1** Bedding, jointing, and differential weathering in existing rock cut.

62 photogrammetry was successfully used to collect the rock discontinuity data. This paper  
 63 summarizes the site geology, describes the process used to obtain the discontinuity data, explains  
 64 how the discontinuity data and digital terrain model were used, and discusses some of the  
 65 advantages of using digital photogrammetry for rock cut slope design.

66  
 67 **PROJECT LOCATION**

68 The project is located on Bald Eagle Mountain, south of Williamsport, Pennsylvania. Bald Eagle  
 69 Mountain forms the northern tip of the Appalachian Mountain Section of Pennsylvania’s Ridge  
 70 and Valley Province (2). The strata underlying Bald Eagle Mountain are tightly folded into an  
 71 anticline plunging to the east and breached to the west. The project is situated in Wind Gap,  
 72 which is the first gap west of the nose of the anticline (Figure 2). The project is located at the  
 73 north end of Wind Gap where Highway 15 curves sharply to the west and descends to its

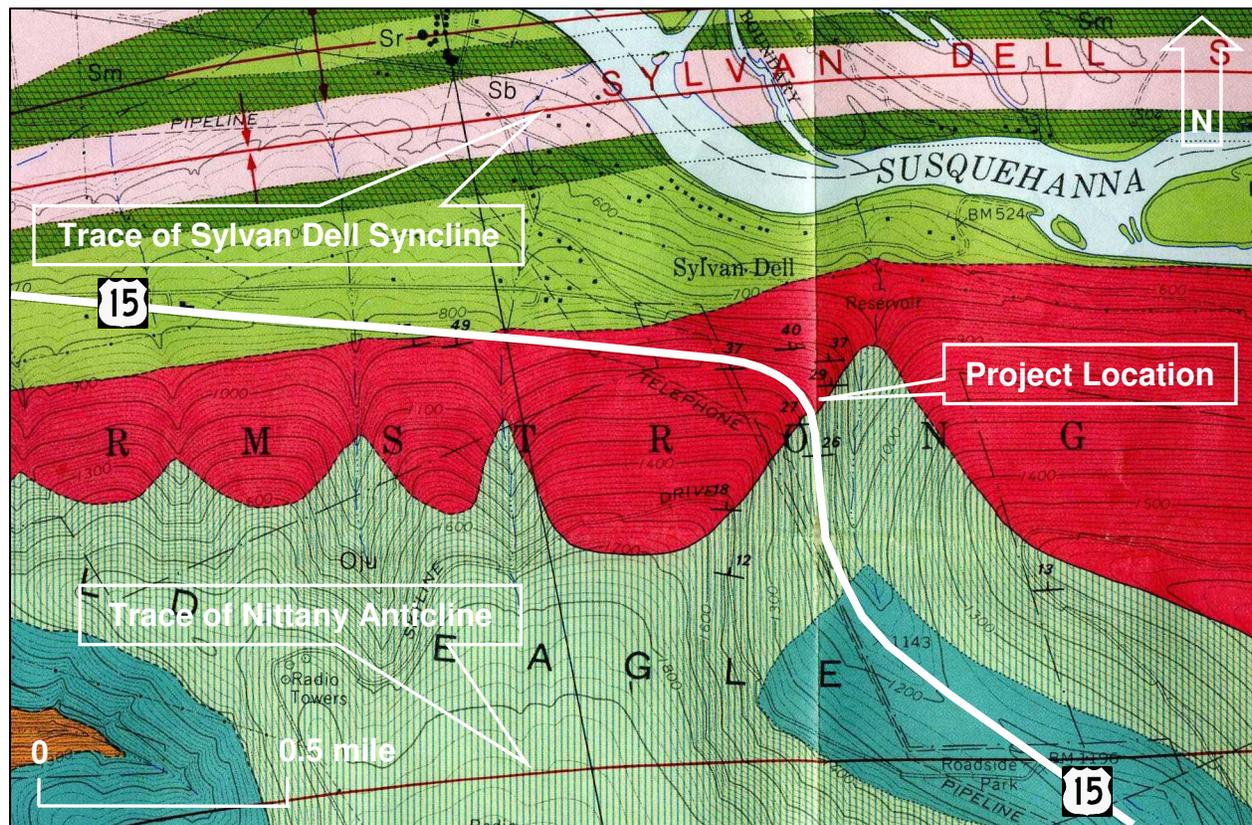


**FIGURE 2 Project location (1).**

74 crossing of the Susquehanna River to the north. The project location provides a remarkable vista  
 75 of the Susquehanna River Valley and the Appalachian Plateau to the north, and PennDOT has  
 76 developed a scenic overlook, with parking and picnic tables, for highway travelers to enjoy the  
 77 view.

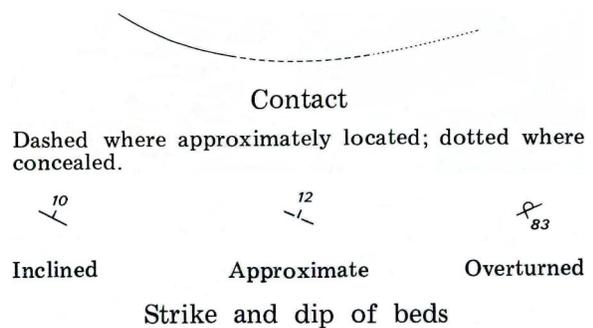
78  
 79 **PROJECT GEOLOGY**

80 According to mapping published by the Pennsylvania Geological Survey (3), the project is  
 81 situated between the axial trace of the Nittany anticline to the south and the Sylan Dell syncline  
 82 to the north (Figure 3). The project straddles the contact between the Juniata Formation of the  
 83 Upper Ordovician system to the south and the Tuscarora Formation of the Lower Silurian system  
 84 to the north (3). According to Faill (4), these rocks formed from sediments deposited in the



**EXPLANATION**

- Bloomsburg Formation
- Mifflintown Formation
- Rose Hill Formation
- Tuscarora Formation
- Upper Unit Juniata Formation
- Lower Unit Juniata Formation
- Bald Eagle Formation



**FIGURE 3 Project geology (3).**

85 Appalachian basin from a source area (the Taconic highlands) located to the southeast of the  
86 basin. The rocks generally consist of fine- to coarse-grained quartzite interbedded with very fine  
87 and fine-grained sandstone, siltstone, and shaly siltstone. The geologic mapping indicates that in  
88 the vicinity of the project, the bedrock strata dip approximately 26 to 37 degrees to the north.  
89 The area above the existing cut is State Forest Land and mantled with colluvium.

90

## 91 **DIGITAL PHOTOGRAMMETRY**

92 Photogrammetry is the practice of determining the geometric properties of objects from  
93 photographic images. Stereophotogrammetry uses photos taken from different locations to  
94 determine an object's coordinates. The technique takes advantage of the fact that sight rays from  
95 an object strike different parts of a camera's image sensor as the location of the camera changes.  
96 Knowing the camera's focal length, the shift in sight rays can be used to triangulate an object's  
97 location. The advent of digital cameras and high-speed computers combined with the  
98 development of sophisticated software has led to the application of digital photogrammetry to  
99 rock face characterization (5, 6, 7).

100 An initial site reconnaissance indicated that the most significant portion of the existing  
101 rock cut could be photographed from a grassy area adjacent to the parking lot of the scenic  
102 overlook. Because of the existing steep slope, challenging access, and high traffic volume,  
103 digital photogrammetry was selected as the method of choice for obtaining the bulk of the rock  
104 discontinuity orientation data required for the cut slope design.

105 Characterizing a rock face using digital photogrammetry involves the following steps:

- 106 1. Calibrate camera/lens
- 107 2. Plan photo shoot
- 108 3. Place survey control points
- 109 4. Take photographs
- 110 5. Match common points – solve free network orientation
- 111 6. Digitize control points – solve absolute orientation
- 112 7. Generate digital terrain model (DTM)
- 113 8. Define features and perform analyses

114

### 115 **Calibrate Camera/Lens**

116 Camera and lens calibration parameters include focal length, radial lens distortion, principal  
117 point offsets, decentring distortion, and pixel scaling factors. Calibration is typically done once  
118 for each camera and lens combination, and re-calibration between projects is not necessary. A  
119 previously calibrated Canon EOS 5D Mark II digital camera with a 50-mm long lens was used  
120 for this project.

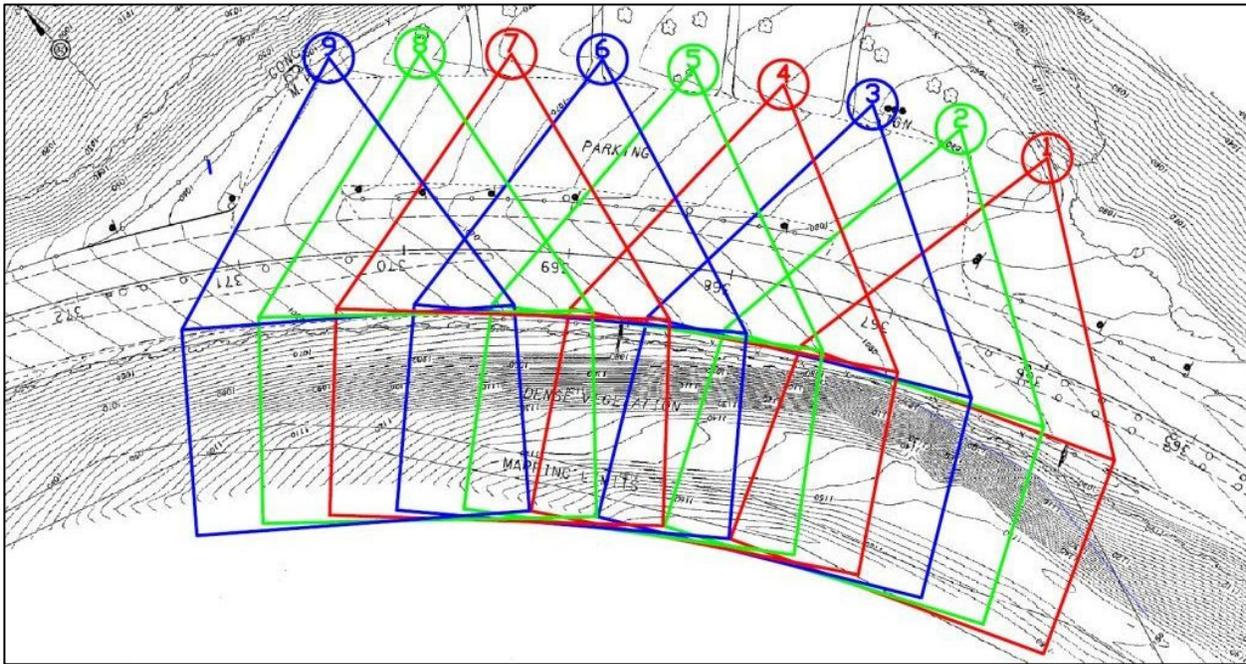
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### 122 **Plan Photo Shoot**

123 The photo shoot is planned based on the type of photogrammetry model to be developed. Three  
124 types of models are typically used in terrestrial photogrammetry:

- 125 1. Simple Convergent Model: Photograph the area or object from two camera locations to  
126 create a stereo pair of images.
- 127 2. Image Fan Model: Multiple photographs are taken obliquely from two locations, usually  
128 with a long focal length lens.
- 129 3. Image Strip Model: Photographs taken head on from multiple locations, usually with a wide  
130 angle lens.

131 Site topography restricted the distance from which the rock face could be photographed  
 132 (i.e., the object distance), so an image strip appeared to be the most feasible model in this case.  
 133 This model usually requires 60 percent horizontal overlap of the images; however, the amount of  
 134 overlap was slightly increased due to the curving nature of the alignment. The plan also sought  
 135 to keep the object distance the same for each camera location (approximately 50 meters). Based  
 136 on the anticipated object distance, a plan for shooting the rock face with a 50-mm lens from nine  
 137 locations was developed (Figure 4).  
 138



**FIGURE 4 Plan for shooting image strip model.**

139

#### 140 **Place Survey Control Points**

141 Prior to taking the photographs, twenty-two 6-inch-diameter control points were spray-painted  
 142 and labeled at various locations on the cut and the existing rockfall fence. PennDOT surveyors  
 143 provided the Northing, Easting, and elevation of each spray-painted control point. Although  
 144 only three control points are required to register the model to a real world coordinate system,  
 145 using more than three control points provides redundancy, which is useful for estimating the  
 146 accuracy of the model and insuring against bad observations.

147

#### 148 **Take Photographs**

149 Photographs were taken on the afternoon November 19, 2010. A tripod was used to steady the  
 150 camera, and a remote switch was used to activate the shutter and minimize movement of the  
 151 camera (Figure 5).

152

#### 153 **Match Common Points – Solve Relative Orientation**

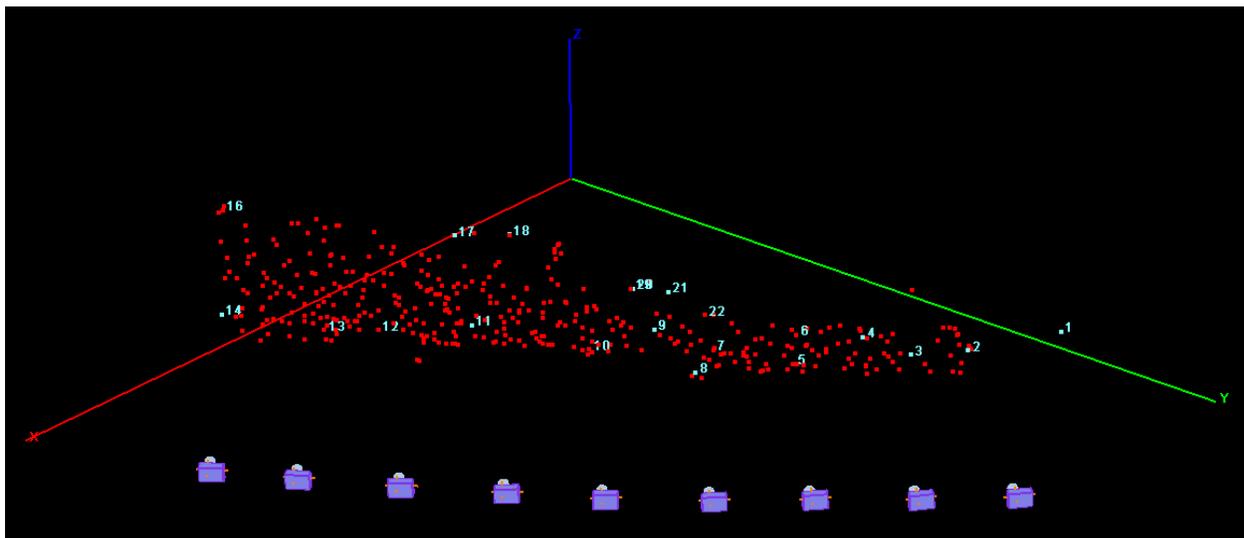
154 Photogrammetry software (3DM Analyst Lite Suite) developed by Adam Technology was used  
 155 to develop the three-dimensional digital model. Common points were identified in pairs of  
 156 overlapping photos, and a bundle adjustment was performed to determine the relative camera  
 157 locations.



**FIGURE 5** Photographing the rock face.

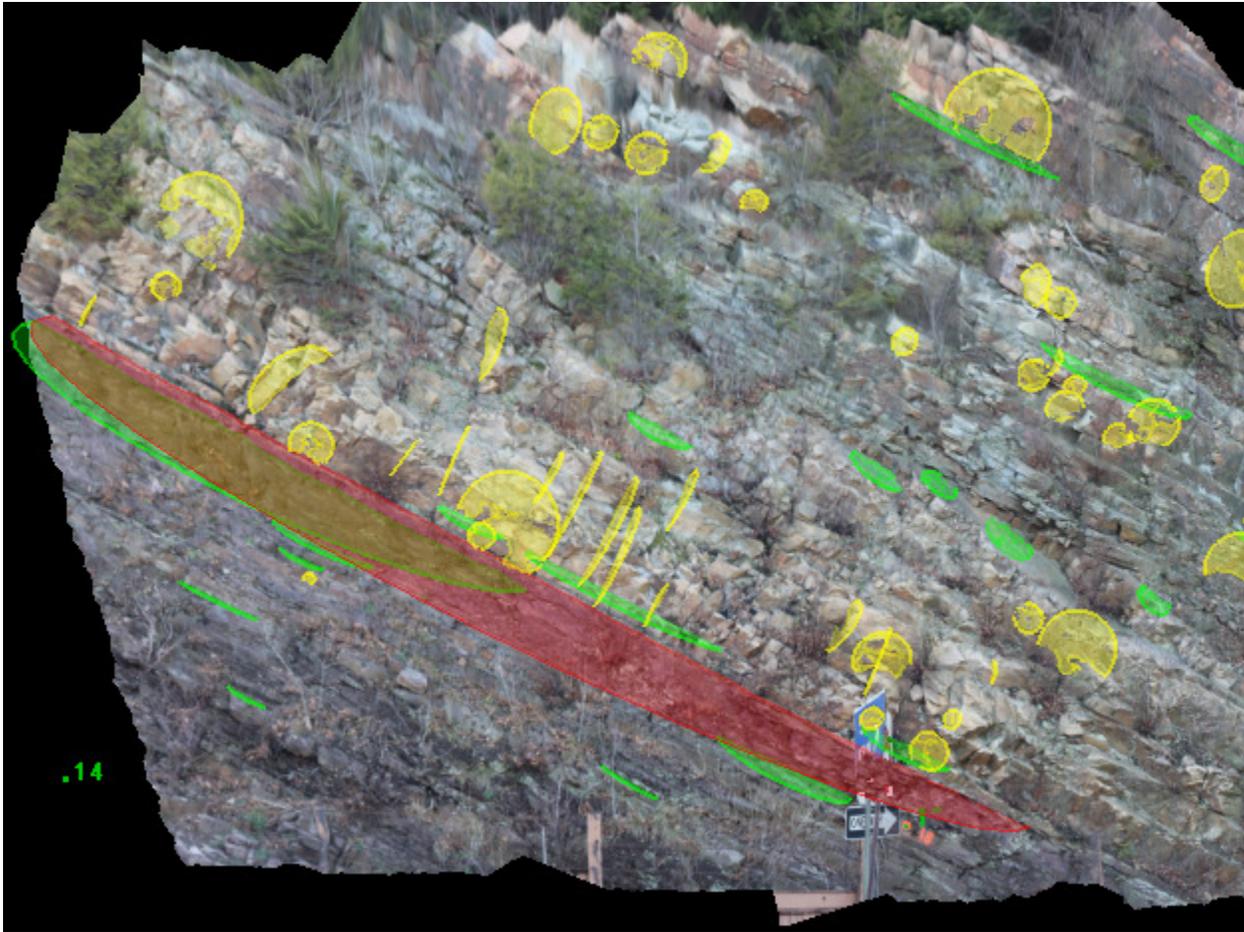
158 **Digitize Control Points – Solve Absolute Orientation**

159 After the free network orientation was solved, surveyed control points were digitized, and an  
 160 absolute orientation was solved to tie the model to a real world coordinate system. Figure 6  
 161 illustrates the plotted locations of the camera stations (purple icons), the matched points (red  
 162 dots), the surveyed control points (teal dots), and the coordinate axes—northing, easting, and  
 163 elevation.



**FIGURE 6** Orientation of nine camera stations, matched points, and control points.





**FIGURE 8** Portion of digital model showing measured bedding joints (green disks); non-bedding joints (yellow disks), and the Tuscarora/Juniata contact (red disk). Red disk is 74.3 feet (22.6 meters) diameter.

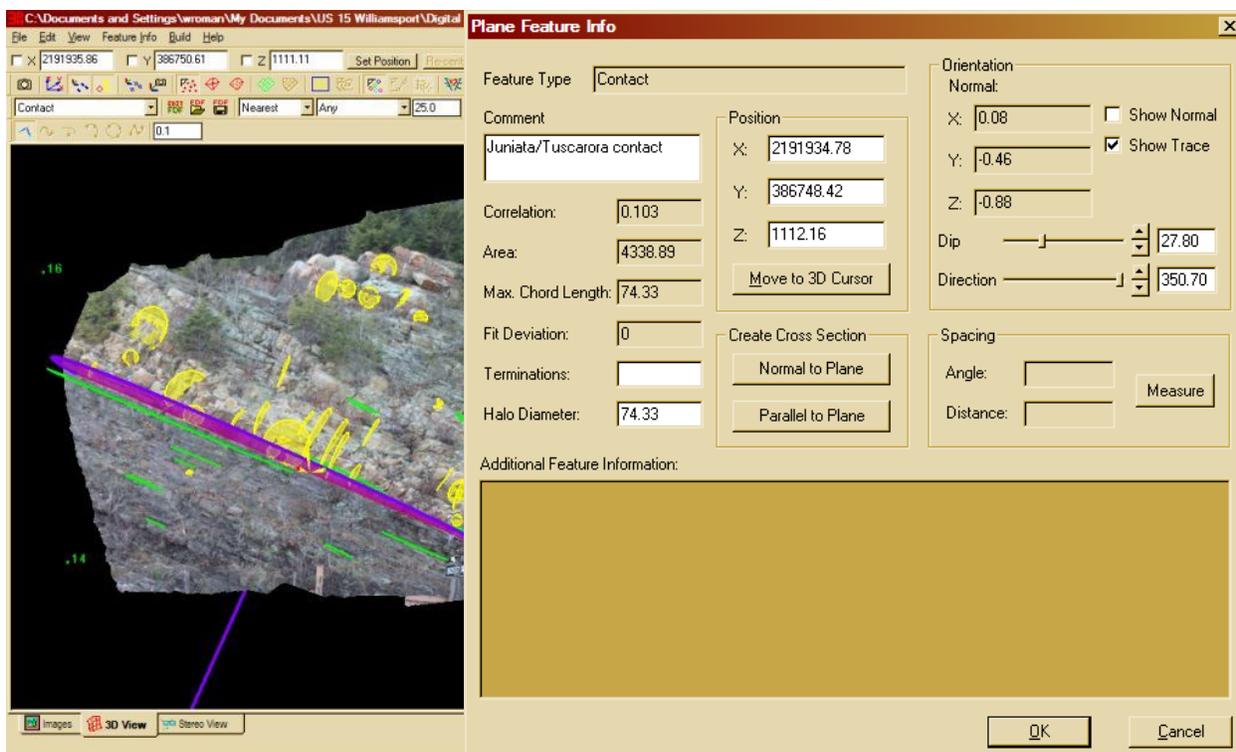
185 tops of some more steeply dipping beds are evident in some locations in the model. These beds  
186 appear to be foreset beds.

187

### 188 **FIELD RECONNAISSANCE**

189 Reconnaissance of the existing rock slope was performed following development of the model in  
190 order to collect additional data and validate the model. An additional 36 rock discontinuities  
191 were measured using a Brunton Geotransit with the magnetic declination set to 11.5 degrees  
192 west. Measurements were collected from areas north and south of the limits of the digital  
193 photogrammetry model and the area behind the existing wall. Some large, conspicuous faces  
194 within the model area were also measured for model validation. Figure 10 provides a stereonet  
195 plot of the dip vectors of the discontinuity orientations measured using the digital photo model  
196 and measured using the Brunton Geotransit. The digital photogrammetry measurements  
197 compare favorably with the manual measurements.

198 Additional reconnaissance was performed to examine the outcrop for clay seams  
199 encountered in test borings performed as part of the subsurface investigation. Projecting the clay  
200 seams to the surface of the digital image was useful in identifying the possible location of the  
201 clay seams in the outcrop face (Figure 11). Reconnaissance also permitted collection of



**FIGURE 9** Dialog box with selected feature information.

202 information not available from the digital imaging, such as measurement of fallen block sizes  
 203 and observation of seepage conditions, joint roughness, weathering, slickensided surfaces, and  
 204 joint in-fillings.

205

## 206 **ROCK FACE CHARACTERIZATION**

207 Discontinuities of two types were identified—bedding joints (including the contact between the  
 208 Tuscarora and Juniata Formations) and two sets of steeply dipping joints. The great circles and  
 209 dip vectors corresponding to the 273 measurements taken on the three joint sets are plotted on  
 210 stereonets in Figure 12. Joint set 1 consists of bedding joints dipping to the north. Joint set 2  
 211 consists of joints striking north-south and dipping steeply to the east and west, and joint set 3  
 212 consists of joints striking east-west and dipping steeply to the south. Histogram analyses of  
 213 bedding dip angle and dip direction and jointing dip angle are also provided in Figure 12.

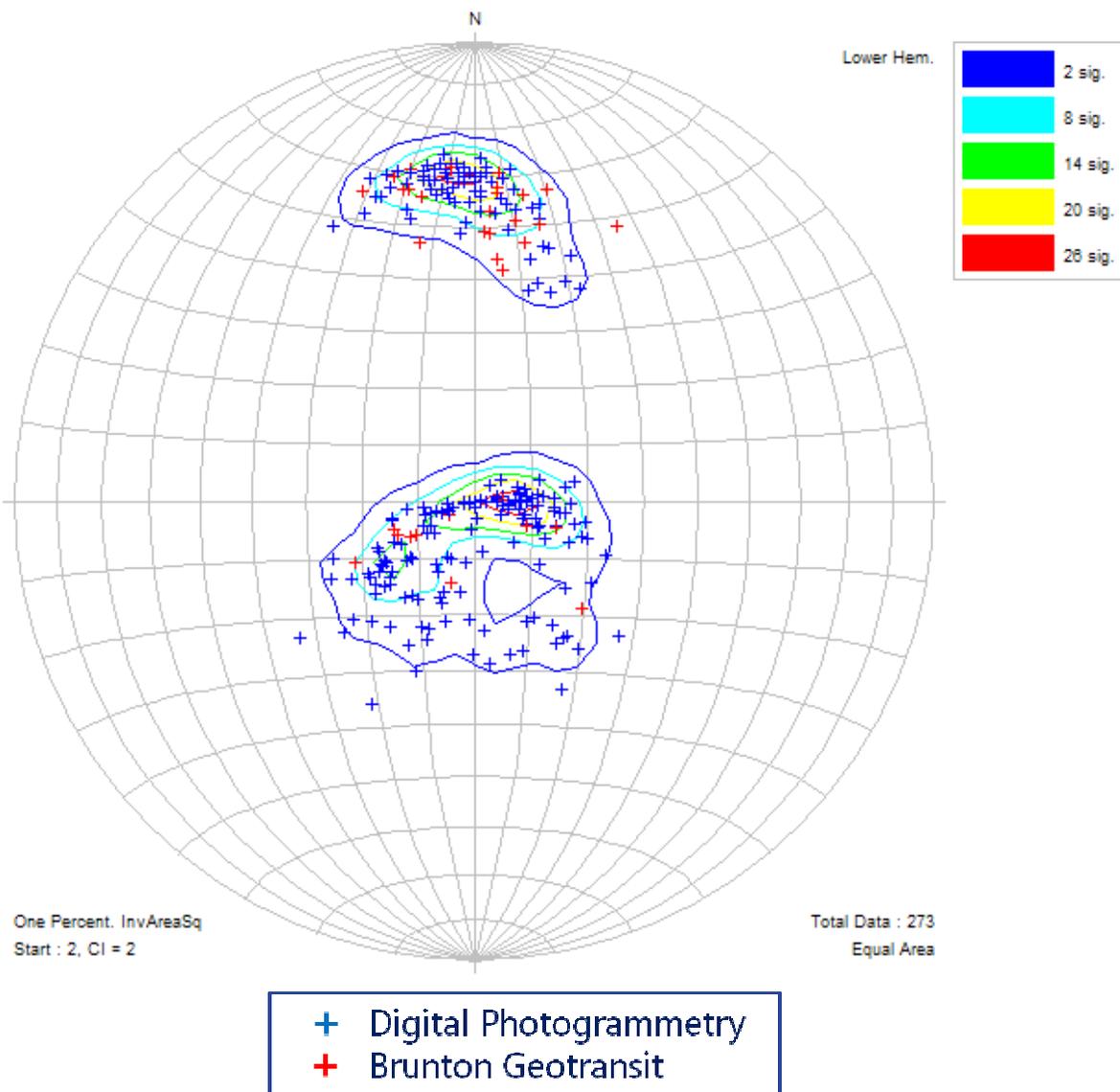
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## 215 **STEREONET ANALYSES**

216 The discontinuity orientation data were analyzed using stereonets to assess the kinematic  
 217 possibility of planar and toppling failures along the measured discontinuities and the kinematic  
 218 possibility of wedge failures along the lines of intersection between the measured discontinuities.  
 219 A friction angle of 27 degrees was used in the analyses given the presence of seeps, as indicated  
 220 by water and ice noted on some bedding planes during the site reconnaissance, and the presence  
 221 of numerous shale and siltstone beds, which tend to deteriorate over time and undercut the  
 222 quartzite beds in the Tuscarora Formation, and to a lesser extent, the sandstone beds of the  
 223 Juniata Formation. During the site reconnaissance, slight displacement of rock blocks was noted  
 224 on bedding surfaces having dips as shallow as 29 degrees.

225 The potential for planar and toppling failure was assessed by using stereonet to plot  
 226 discontinuity dip vectors and to identify the critical area associated with varying cut slopes and  
 227 slope directions along the curved highway alignment. To assess wedge failures, a matrix of  
 228 vector cross product equations was solved to determine the lines of intersections between  
 229 bedding and jointing and between the east-west and north-south striking joints. A contour plot of  
 230 the lines of intersections was used to assess the kinematic potential for wedge failure for  
 231 alternate cut slope designs (Figure 13).

232 The stereonet analyses were generally favorable with respect to the principal components  
 233 of bedding and jointing; however the analyses indicated planar and wedge failures are  
 234 kinematically possible at the fringes of the discontinuity sets toward the northern end of the  
 235 study area, and toppling is a possibility, particularly in the steeper portions of the northern half of  
 236 the study area.  
 237



**FIGURE 10 Comparison of digital photogrammetry and manual measurements.**



**FIGURE 11** Weathered shale bed possibly correlating with clay seam encountered in test boring.

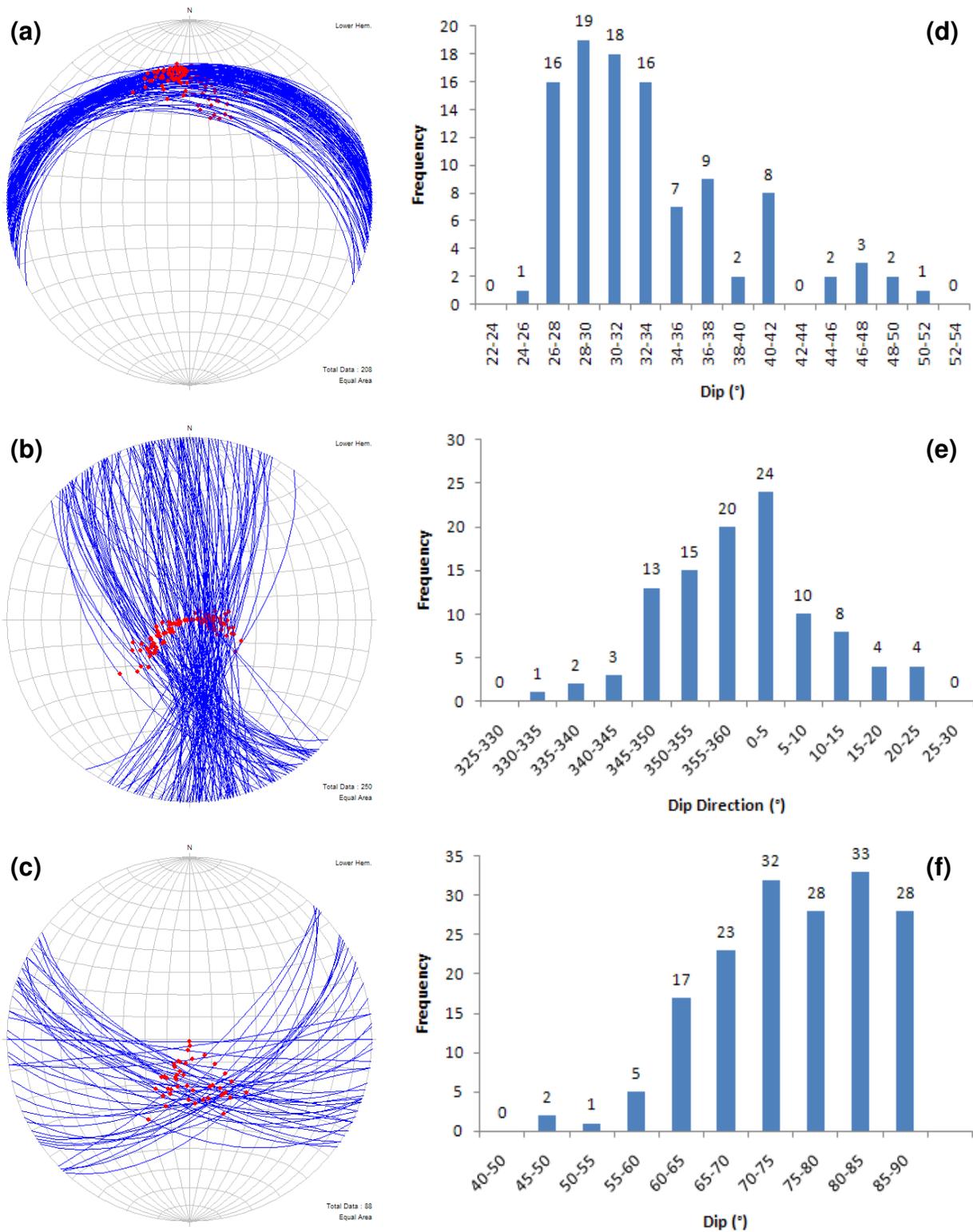
238 **SUBSURFACE INVESTIGATION**

239 Six core borings were drilled. Overall core recovery was 96.3 percent. Core recovery was  
240 slightly higher in the Juniata Formation (98.2 percent) than in the Tuscarora Formation  
241 (95.5 percent). Overall Rock Quality Designation (RQD) was 65.8 percent, which indicates  
242 generally fair quality rock. RQD was slightly higher in the Juniata Formation (68.1 percent) than  
243 in the Tuscarora Formation (64.8 percent). Boring logs indicate bedding dips ranging from 22 to  
244 28 degrees in the Juniata Formation and generally from 16 to 32 degrees in the Tuscarora  
245 Formation; however, dips as steep as 40 degrees were sometimes noted in the latter formation.  
246 These observations are generally consistent with observations from the digital photogrammetry  
247 model and manual measurements. Spacing and orientation of non-bedding joints noted in the  
248 boring logs are also generally consistent with observations from the 3D model and from site  
249 reconnaissance.

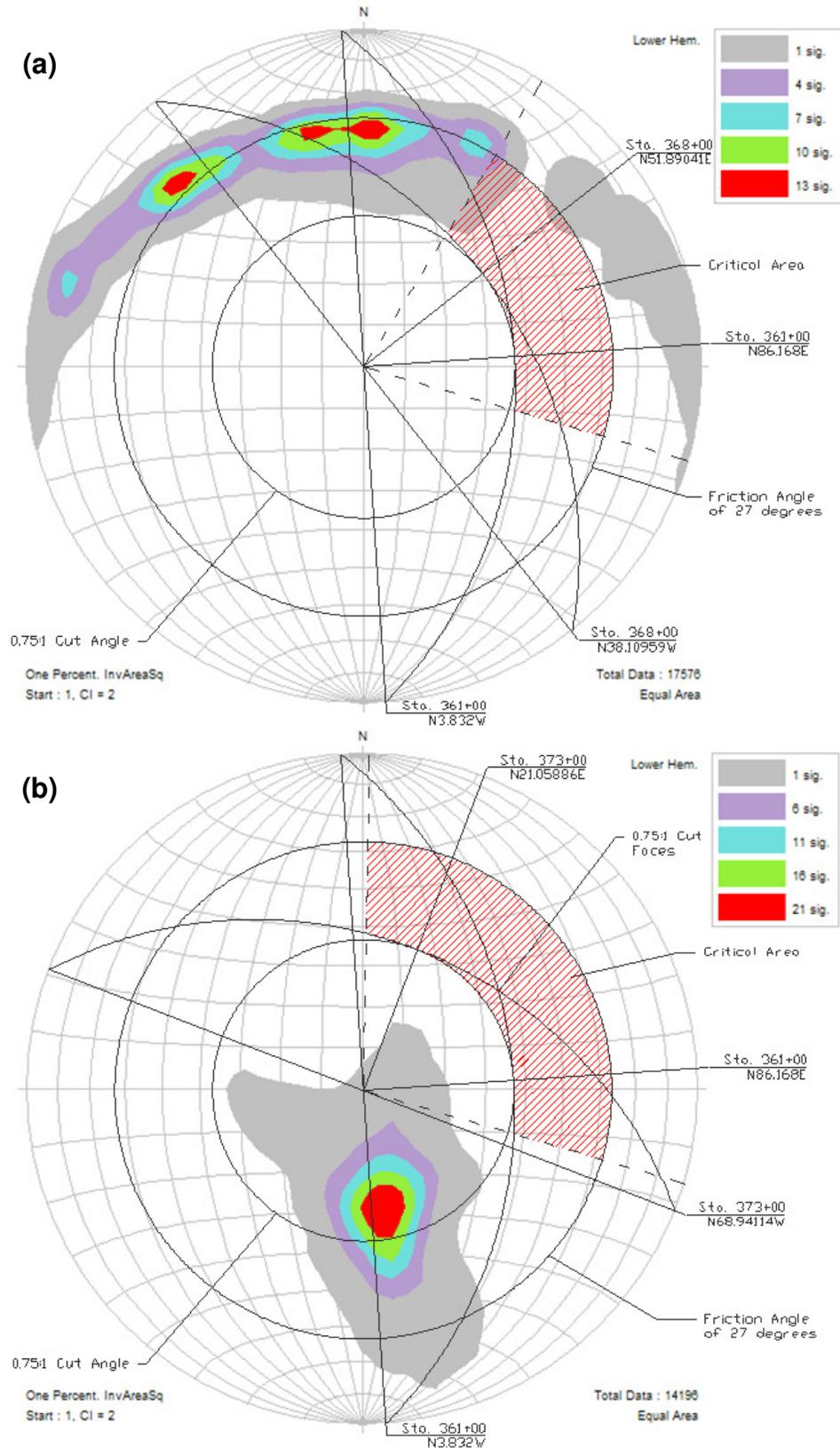
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251 **OTHER ANALYSES**

252 In addition to the discontinuity analyses, other analyses factored into the rock cut slope design  
253 included laboratory analyses of clay samples from test borings (residual shear and fully softened  
254 direct shear tests), stability calculations using the factor of safety formula of Hoek and Bray (8),  
255 and rockfall catchment zone analyses using the Colorado Rockfall Simulation Program (9), and  
256 the Ritchie ditch design chart (10). The stability calculations considered the potential sliding  
257 (plane) failure occurring along clay seams and factored in water pressure building up along the  
258 clay seams and within a tension fracture forming the upper release surface for the sliding rock



**FIGURE 12** Great circles (blue lines) and dip vectors (red dots) of (a) joint set 1 (bedding), (b) joint set 2, and (c) joint set 3. Histogram analyses of (d) bedding dip angle, (e) bedding dip direction, and (f) jointing dip angle.



**FIGURE 13 Kinematic analyses for wedge failures using contour density plots of lines of intersections between (a) bedding and jointing, and (b) joint sets 2 and 3.**

261 mass. The stability calculations used a cohesion value of 300 pounds/foot<sup>2</sup> (0.29 kPa) and a  
262 friction angle of 20 degrees.

263

### 264 **ROCK CUT SLOPE DESIGN**

265 Rock cut slopes ranging from 1.5H:1V to 1H:1V were recommended along various portions of  
266 the alignment. In transition zones between the recommended rock cut slopes, it was  
267 recommended that smooth, linear transitions be provided and that adverse rock slopes dipping  
268 between N30°W and N30°E be avoided. Although stereonet analyses indicated steeper cut  
269 slopes were possible in portions of the cut, these areas were not of sufficient extent to warrant  
270 steepening the proposed cut slope, especially since steepening the cut slope tended to create  
271 transition zones having adverse orientations.

272 A rock catchment basin was recommended because of the remaining rockfall potential  
273 and instabilities that may develop over time as a result of natural rock weathering processes,  
274 including free-thaw cycles, undercutting due to differential weathering of the shale and siltstone  
275 beds, and leveraging by vegetation. Horizontal drain holes were recommended to improve the  
276 factor of safety with respect to sliding along clay seams encountered in test borings. The drain  
277 hole orientation was optimized using the vector dot product formula and average joint  
278 orientations and typical spacing. The rock cut portion of the project is expected to be completed  
279 in 2012.

280

### 281 **APPLICATION OF DIGITAL PHOTOGRAMMETRY**

282 Digital photogrammetry worked quite well on this project. The discontinuity measurements  
283 from the digital photogrammetry model were used in the stereonet analyses of the kinematic  
284 potential for plane, wedge, and toppling failures. The measurements were also used in  
285 optimizing the azimuth of horizontal drains proposed to reduce water pressure within the rock  
286 mass and improve cut slope stability. Having the coordinates of each measurement permitted  
287 analysis of the variability of bedding dip angle and dip direction along the curving highway  
288 alignment. The digital model was also useful for locating the possible outcrops of clay seams  
289 encountered in test borings.

290 This project illustrated some of the advantages of using digital photogrammetry for rock  
291 cut slope design. Specific advantages include the following:

- 292 1. Data can be collected safely from challenging to reach areas with no rappelling or free  
293 climbing.
- 294 2. Exposure to traffic, rockfalls, and inclement weather is significantly reduced.
- 295 3. A robust set of measurements can be collected in a short period of time.
- 296 4. There is no need to set up and measure traverses since the software provides coordinates of  
297 each measurement.
- 298 5. Discontinuities are measured across a greater area of their extent than can be measured by  
299 hand.
- 300 6. Discontinuities with limited exposure are easily measured by digitizing their trace across  
301 the outcrop model.
- 302 7. Measurements are fitted to the digital image of the rock face, which can be rotated and  
303 viewed edge-on to assess the closeness of the fit.
- 304 8. Having the coordinates of each discontinuity measurement facilitates analysis of the  
305 variability of bedding dip and dip direction along the roadway alignment.

- 306 9. Human error in recording the measurements is reduced since the measurements are  
307 recorded by the computer.
- 308 10. Shallow dipping (<5 degrees) joints, which can be very challenging to measure with a  
309 compass, can be easily measured by digitizing their trace along the digital model.
- 310 Although useful for quickly and safely collecting discontinuity orientation data required  
311 for kinematic analyses, digital photogrammetry may not permit measurement of fallen block  
312 sizes and observation of seepage conditions, joint roughness, weathering, slickensided surfaces,  
313 and joint in-fillings needed for other analyses factored into the design of a rock cut.

314

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